Lect. 15: Second-Order Passive Filters (S&S 12.5)

2nd-order filter
$$T(s) = \frac{a_2 S^2 + a_1 S^1 + a_0}{S^2 + b_1 S^1 + b_0} = \frac{a_2 (s - z_1)(s - z_2)}{(s - p_1)(s - p_2)}$$

If p_1 , p_2 are real,

→ 2nd-order filters can be easily made by cascading two 1st-order filters

Consider T(s) with complex poles

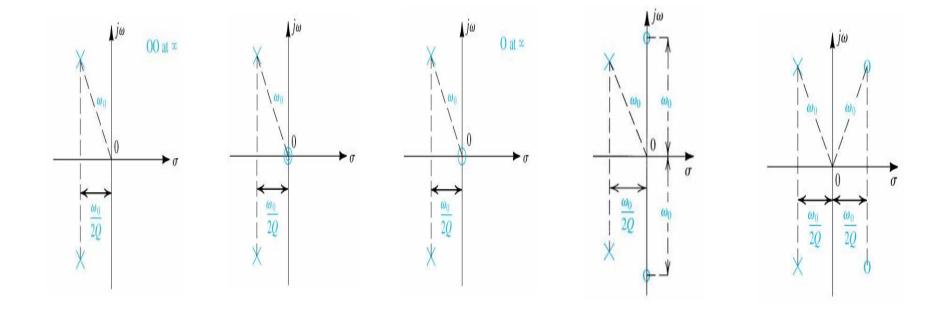
$$T(s) = \frac{a_2 s^2 + a_1 s + a_0}{s^2 + (\omega_0 / Q)s + \omega_0^2}$$

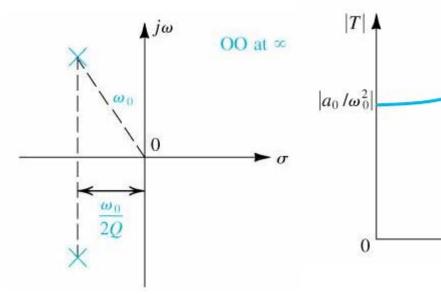
$$p_1, p_2 = -\frac{\omega_0}{2Q} \pm j\omega_0 \sqrt{1 - (1/4Q^2)}$$
(Q > ½)

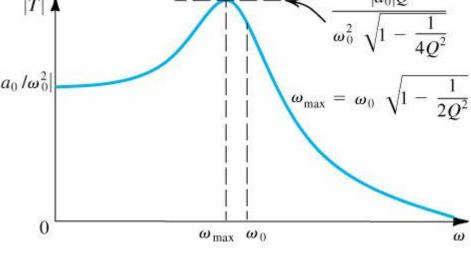
tics! $\frac{j\omega}{\omega_0}$ s plane

Depending on zero locations, various filter characteristics!

Second-order filter pole-zero diagrams







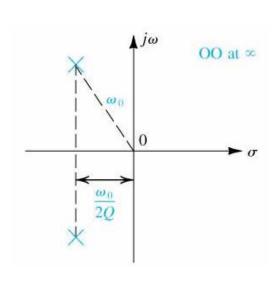
LP Filter

$$T(s) = \frac{\omega_0}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$$

At
$$\omega = \omega_0$$
, $|T| = |a_0/\omega_0^2| Q$

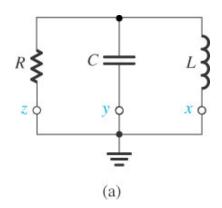
Larger Q → More peaking

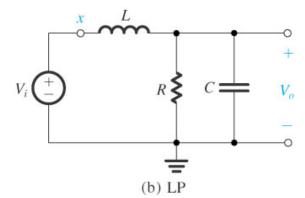
How to realize passive second-order LP filter



$$T(s) = \frac{a_0}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$$

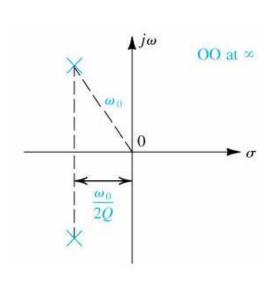
Use LCR



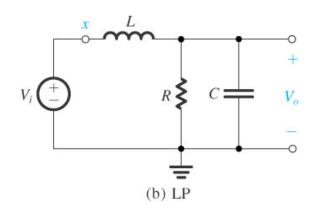


→ Two zeros at s infinity

How to realize passive second-order LP filter



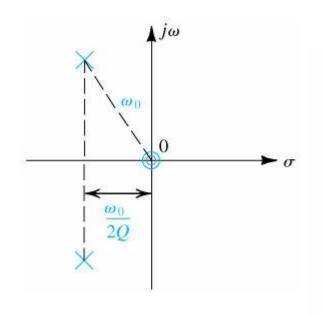
$$T(s) = \frac{a_0}{s^2 + s\frac{\omega_0}{O} + \omega_0^2}$$

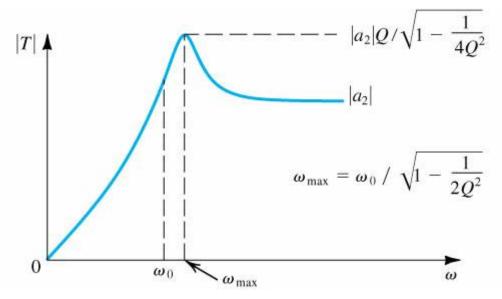


$$T(s) = \frac{V_0}{V_i} = \frac{Z_2}{Z_1 + Z_2} = \frac{Y_1}{Y_1 + Y_2} = \frac{1/sL}{(1/sL) + sC + (1/R)}$$

$$= \frac{1/LC}{s^2 + s(1/CR) + (1/LC)} = \frac{\omega_0^2}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$$

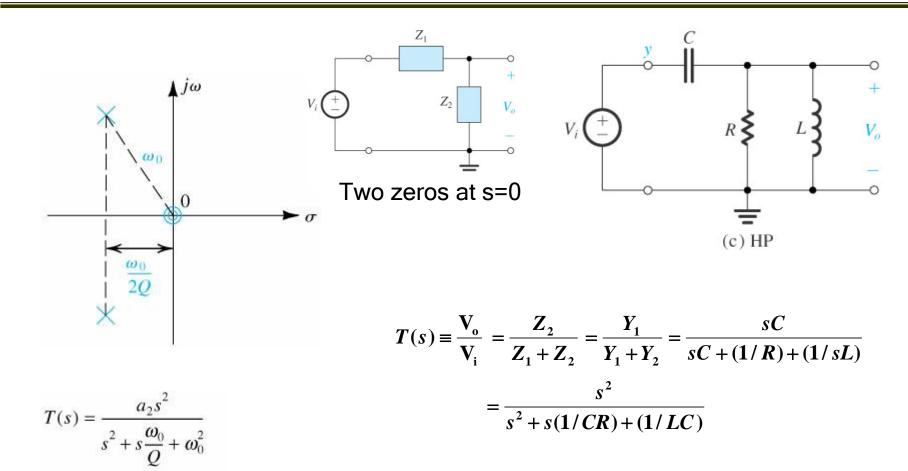
$$\omega_0 = \frac{1}{\sqrt{LC}} \qquad \frac{\omega_0}{Q} = \frac{1}{CR} \qquad Q = \omega_0 CR = \sqrt{\frac{C}{L}}R$$





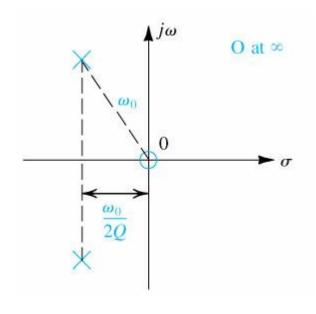
$$T(s) = \frac{a_2 s^2}{s^2 + s \frac{\omega_0}{O} + \omega_0^2}$$

HP Filter

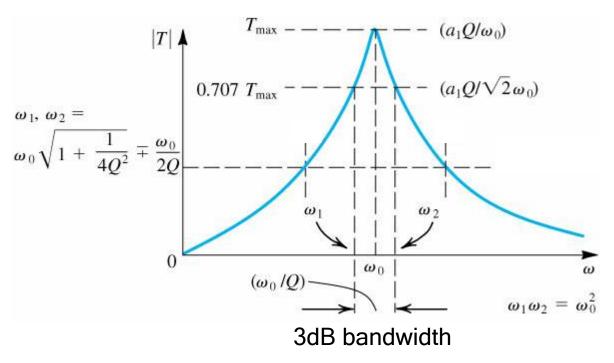


Same pole characteristics as LP filter: ω_0 Q identical



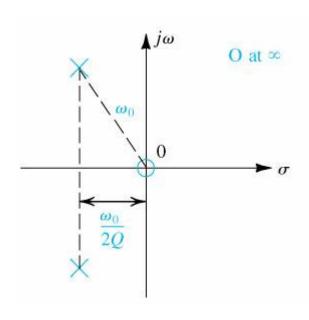


$$T(s) = \frac{a_1 s}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$

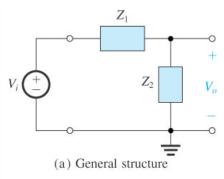


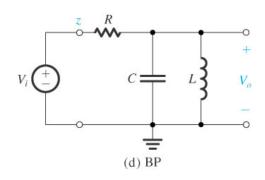
BP Filter

Large Q → Sharper response



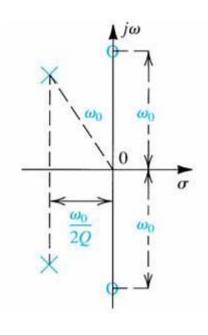
$$T(s) = \frac{a_1 s}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$



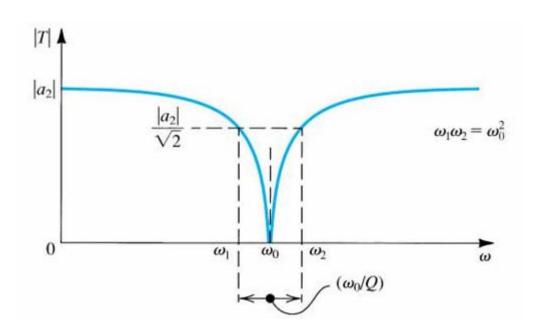


$$T(s) = \frac{V_o}{V_i} = \frac{Y_1}{Y_1 + Y_2} = \frac{1/R}{(1/R) + sC + (1/sL)}$$
$$= \frac{s(1/RC)}{s^2 + s(1/RC) + (1/LC)}$$

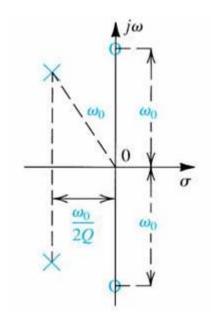
$$Q = \omega_0 CR = \sqrt{\frac{C}{L}}R$$



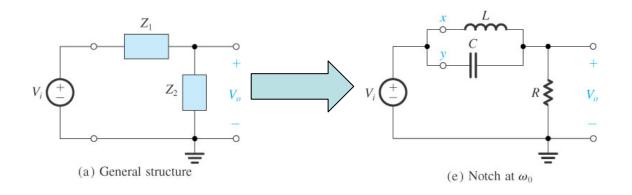
$$T(s) = a_2 \frac{s^2 + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$



Band-Rejection or Notch Filter

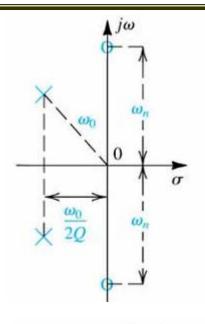


$$T(s) = a_2 \frac{s^2 + \omega_0^2}{s^2 + s\frac{\omega_0}{\Omega} + \omega_0^2}$$



$$Z_1 = \frac{sL \cdot \frac{1}{sC}}{sL + \frac{1}{sC}} = \frac{sL}{1 + s^2LC}$$

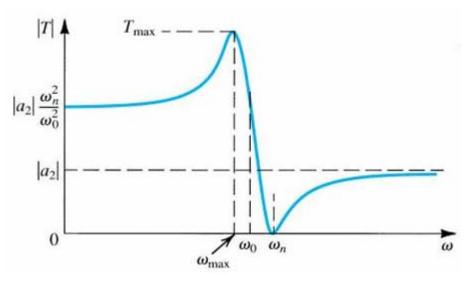
$$T(s) = a_2 \frac{s^2 + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2} \qquad T(s) = \frac{\mathbf{V}_0}{\mathbf{V}_i} = \frac{\mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2} = \frac{R}{\frac{sL}{1 + s^2LC} + R} = \frac{s^2 + (1/LC)}{s^2 + s(1/RC) + (1/LC)}$$



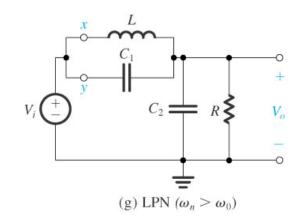
$$T(s) = a_2 \frac{s^2 + \omega_n^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$$
$$\omega_n \ge \omega_0$$

DC gain =
$$a_2 \frac{\omega_n^2}{\omega_0^2}$$

High-frequency gain = a_2

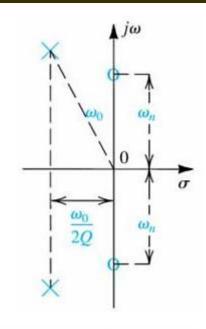


Low-Pass Notch Filter



$$T(s) = \frac{s^2 + (1/LC_1)}{s^2 + s \frac{1}{(C_1 + C_2)R} + \frac{1}{L(C_1 + C_2)}}$$

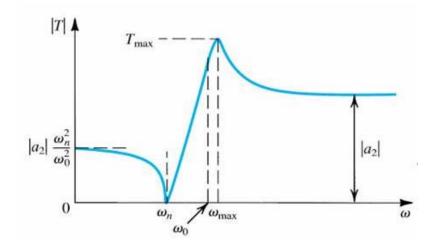




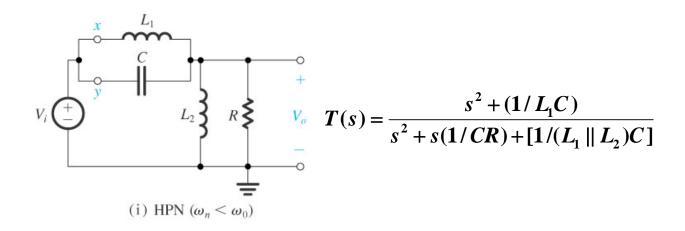
$$T(s) = a_2 \frac{s^2 + \omega_n^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$
$$\omega_n \le \omega_0$$

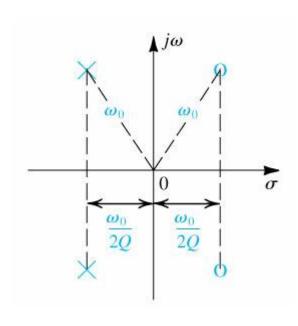
DC gain =
$$a_2 \frac{\omega_n^2}{\omega_0^2}$$

High-frequency gain = a_2



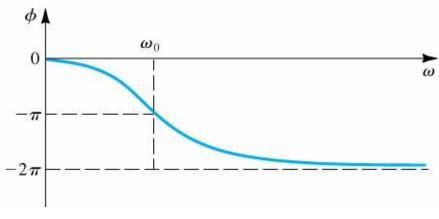
High-Pass Notch Filter

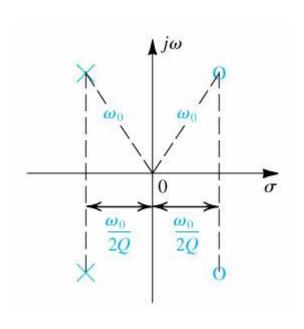




$$T(s) = a_2 \frac{s^2 - s \frac{\omega_0}{Q} + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$







$$T(s) = a_2 \frac{s^2 - s \frac{\omega_0}{Q} + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$

$$T(s) = \frac{s^2 - s(\omega_0/Q) + \omega_0^2}{s^2 + s(\omega_0/Q) + \omega_0^2} = 1 - \frac{s2(\omega_0/Q)}{s^2 + s(\omega_0/Q) + \omega_0^2}$$
$$= 2\left(\frac{1}{2} - \frac{s(\omega_0/Q)}{s^2 + s(\omega_0/Q) + \omega_0^2}\right)$$

